Prevailing torque type steel nuts — Mechanical and performance properties (ISO 2320:2008)

ICS 21.060.20



National foreword

This British Standard is the UK implementation of EN ISO 2320:2008. It supersedes BS EN ISO 2320:1998 which is withdrawn.

The UK participation in its preparation was entrusted to Technical Committee FME/9/1, Mechanical properties of fasteners.

A list of organizations represented on this committee can be obtained on request to its secretary.

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Écrous autofreinés en acier - Caractéristiques mécaniques et performances (ISO 2320:2008)

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Management Centre: rue de Stassart, 36 B-1050 Brussels

Foreword

This document (EN ISO 2320:2008) has been prepared by Technical Committee ISO/TC 2 "Fasteners" in collaboration with Technical Committee CEN/TC 185 "Fasteners" the secretariat of which is held by DIN.

This European Standard shall be given the status of a national standard, either by publication of an identical text or by endorsement, at the latest by May 2009, and conflicting national standards shall be withdrawn at the latest by May 2009.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. CEN [and/or CENELEC] shall not be held responsible for identifying any or all such patent rights.

This document supersedes EN ISO 2320:1997.

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Endorsement notice

The text of ISO 2320:2008 has been approved by CEN as a EN ISO 2320:2008 without any modification.

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

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ISO 2320 was prepared by Technical Committee ISO/TC 2, Fasteners, Subcommittee SC 1, Mechanical properties of fasteners.

This fourth edition cancels and replaces the third edition (ISO 2320:1997), which has been technically revised. It also incorporates the Technical Corrigendum ISO 2320:1997/Cor.1:2006.

Prevailing torque type steel nuts — Mechanical and performance properties

1 Scope

This International Standard specifies the mechanical and performance properties for prevailing torque type steel nuts when tested at an ambient temperature range of +10 °C to +35 °C. It includes a single test to determine the prevailing torque properties (performance properties) and/or the torque/clamp force properties.

This International Standard applies to prevailing torque all metal type nuts and prevailing torque non-metallic insert type nuts:

- a) with triangular ISO thread according to ISO 68-1;
- b) with diameter/pitch combination according to ISO 261 and ISO 262;
- with coarse pitch thread M3 to M39 and mechanical properties according to ISO 898-2;
- d) with fine pitch thread M8×1 to M39×3 and mechanical properties according to ISO 898-6;
- e) within the temperature range of -50 °C to +150 °C for prevailing torque all metal type nuts;
- NOTE 1 See Clause 7, paragraph 3.
- f) within the temperature range of -50 °C to +120 °C for prevailing torque non-metallic insert type nuts.
- NOTE 2 See Clause 7, paragraph 4.

2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 273:1979, Fasteners — Clearance holes for bolts and screws

ISO 898-1, Mechanical properties of fasteners made of carbon steel and alloy steel — Part 1: Bolts, screws and studs

ISO 898-2, Mechanical properties of fasteners — Part 2: Nuts with specified proof load values — Coarse thread

ISO 898-6, Mechanical properties of fasteners — Part 6: Nuts with specified proof load values — Fine pitch thread

ISO 965-2, ISO general purpose metric screw threads — Tolerances — Part 2: Limits of sizes for general purpose external and internal screw threads — Medium quality

ISO 16047, Fasteners — Torque/clamp force testing

3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 16047 and the following apply.

3.1

prevailing torque type nut

nut which is not free-running on a mating thread by virtue of a self-contained prevailing torque feature, and which provides a degree of resistance to rotation independent of clamping or compression forces

3.2

prevailing torque developed by the nut

torque necessary to rotate the nut on its mating externally threaded component and with no axial force in the mating component

3.3

prevailing-on torque

torque to rotate the nut on its mating externally threaded component with the torque measured while the nut is in motion and with no clamp force

3.4

prevailing-off torque

torque to rotate after backing off the nut until the removal of the clamp force in the externally threaded component in the following 360° rotation of the nut

3.5

prevailing torque all metal type nut

nut which has a one piece or a multiple piece metal construction and derives its prevailing torque characteristics from a controlled distortion of the nut thread and/or body or from metallic insert(s)

3.6

prevailing torque non-metallic insert type nut

nut which has a multiple piece construction and derives its prevailing torque characteristics from insert(s) of non-metallic material located and retained in the nut

3.7

seating point

point in the tightening process where clamp force first appears

4 Symbols

For the purpose of this International Standard, the following symbols apply together with those defined in ISO 16047.

Symbol Designation

| d | nominal diameter |
|-----------------|--|
| d_4 | diameter of the hole of the fixture |
| F_{P} | proof load |
| F ₆₅ | lower load limit for the evaluation of the coefficient of total friction at 65 % of $F_{\mbox{\scriptsize P}}$ |
| F ₇₅ | upper load limit for the evaluation of the coefficient of total friction at 75 % of $F_{\rm P}$ |
| F ₈₀ | test clamp force (shut-down force for the tightening process) at 80 % of $F_{\rm P}$ |
| P | pitch of the thread |
| T_{FV} | prevailing-on torque, in newton metres |

| T_{Fd} | prevailing-off torque, in newton metres |
|------------------------|---|
| T ₆₅ | lower torque limit for the evaluation of the coefficient of total friction at F_{65} |
| <i>T</i> ₇₅ | upper torque limit for the evaluation of the coefficient of total friction at ${\cal F}_{75}$ |
| T ₈₀ | test torque corresponding to 80 % of the proof load, in newton metres (see Tables 1 to 8) |
| μ_{tot} | coefficient of total friction |

5 Thread

Threads for prevailing torque type nuts shall be in accordance with ISO 965-2 except for the prevailing torque feature:

- a) for prevailing torque non-metallic insert type nuts, the GO gauge shall be suitable for free installation (by hand) until it is seated against the prevailing torque feature;
- for prevailing torque all metal type nuts, the GO gauge shall be suitable for free installation (by hand) to one pitch at least.

6 Lubrication

At the option of the manufacturer a lubricant may be applied to the manufacturing lot to fulfil the performance requirements.

7 Mechanical properties of prevailing torque type nuts

The mechanical properties of prevailing torque type nuts shall conform to ISO 898-2 or ISO 898-6.

With regard to proof load, the test method specified in 9.2 shall apply.

For prevailing torque all metal type nuts, users should consult an experienced fastener materials expert for temperatures outside the range of -50 °C to +150 °C to determine appropriate choices for a given application.

For prevailing torque non-metallic insert type nuts, use at or near the temperature limits of -50 °C and +120 °C may reduce the prevailing torque capability and may require the use of an adequate non-metallic material. Users should consult an experienced fastener materials expert for temperatures outside the range of -50 °C to +120 °C to determine appropriate choices for a given application.

8 Performance requirements for prevailing torque properties

The prevailing-on torque shall not exceed the value specified for the applicable nut in Tables 1 to 8.

The prevailing-off torque shall exceed the value specified for the applicable nut in Tables 1 to 8.

For delivery inspection, the 1st installation/removal test applies, unless otherwise agreed.

For initial type testing and in case of dispute, a 5th removal test shall also be applied unless otherwise agreed.

Prevailing torque performance decreases as a function of the number of reuses; the consumer should take into consideration the consequences of the decreased performance before any reuse of the nut.

By request of the customer, a temperature resistance test for prevailing torque non-metallic insert type nuts as given in Annex A may be carried out.

Paragraphs 3 and 4 of Clause 7 also apply to performance requirements.

Table 1 — Test clamp force and prevailing torques for prevailing torque type nuts of property class 04

| Thread | Test clamp force Clamp force of total friction coefficient $\mu_{\mathrm{tot}}^{\mathrm{b}}$ | | Prevailing torque N⋅m | | | |
|----------|--|-----------------------------------|-----------------------------------|-------------------|------------------|--------------------------------|
| d P | F ₈₀ a | Upper limit | Lower limit | | | |
| u r | N | | | 1st installation | 1st removal | 5th removal |
| | N | F ₇₅ ^c N | F ₆₅ ^d N | $T_{Fv,max}^{}e}$ | $T_{Fd,min}^{}}$ | $T_{Fd,min}^{\qquad \qquad f}$ |
| M3 | 1 528 | 1 433 | 1 242 | 0,43 | 0,12 | 0,08 |
| M4 | 2 672 | 2 505 | 2 171 | 0,9 | 0,18 | 0,12 |
| M5 | 4 320 | 4 050 | 3 510 | 1,6 | 0,29 | 0,2 |
| M6 | 6 112 | 5 730 | 4 966 | 3 | 0,45 | 0,3 |
| M7 | 8 800 | 8 250 | 7 150 | 4,5 | 0,65 | 0,45 |
| M8 | 11 120 | 10 425 | 9 035 | - 6 | 0.05 | 2.2 |
| M8×1 | 11 920 | 11 175 | 9 685 | | 0,85 | 0,6 |
| M10 | 17 600 | 16 500 | 14 300 | | | |
| M10×1,25 | 18 640 | 17 475 | 15 145 | 10,5 | 1,5 | 1 |
| M10×1 | 19 600 | 18 375 | 15 925 | | | |
| M12 | 25 600 | 24 000 | 20 800 | | 2,3 | |
| M12×1,5 | 26 800 | 25 125 | 21 775 | 15,5 | | 1,6 |
| M12×1,25 | 28 000 | 26 250 | 22 750 | · | | |
| M14 | 34 960 | 32 775 | 28 405 | | 3,3 | |
| M14×1,5 | 38 000 | 35 625 | 30 875 | 24 | | 2,3 |
| M16 | 47 760 | 44 775 | 38 805 | | | 3 |
| M16×1,5 | 50 800 | 47 625 | 41 275 | 32 | 4,5 | |
| M18 | 58 400 | 54 750 | 47 450 | | | 1.0 |
| M18×1,5 | 65 360 | 61 275 | 53 105 | 42 | 6 | 4,2 |
| M20 | 74 480 | 69 825 | 60 515 | _, | | |
| M20×1,5 | 82 720 | 77 550 | 67 210 | - 54 | 7,5 | 5,3 |
| M22 | 92 080 | 86 325 | 74 815 | 00 | 0.5 | 0.5 |
| M22×1,5 | 101 200 | 94 875 | 82 225 | 68 | 9,5 | 6,5 |
| M24 | 107 280 | 100 575 | 87 165 | 00 | 44.5 | _ |
| M24×2 | 116 720 | 109 425 | 94 835 | - 80 | 11,5 | 8 |
| M27 | 139 520 | 130 800 | 113 360 | 0.4 | 40.5 | 40 |
| M27×2 | 150 800 | 141 375 | 122 525 | 94 | 13,5 | 10 |
| M30 | 170 560 | 159 900 | 138 580 | 400 | 40 | 40 |
| M30×2 | 188 800 | 177 000 | 153 400 | 108 | 16 | 12 |
| M33 | 210 960 | 197 775 | 171 405 | 122 | 40 | |
| M33×2 | 231 360 | 216 900 | 187 980 | | 18 | 14 |
| M36 | 248 400 | 232 875 | 201 825 | 400 | 6.4 | 40 |
| M36×3 | 262 960 | 246 525 | 213 655 | 136 | 21 | 16 |
| M39 | 296 720 | 278 175 | 241 085 | 450 | 60 | 40 |
| M39×3 | 313 120 | 293 550 | 254 410 | 150 | 23 | 18 |

The clamp force for property class 04 nuts is equal to 80 % of the proof load of property class 04 nuts for 3 mm $\leq d \leq$ 39 mm. Proof loads for nuts are given in ISO 898-2 and ISO 898-6.

b See Annex B.

The value of the upper limit of the clamp force is equal to 75 % of the proof load, see Annex B.

d The value of the lower limit of the clamp force is equal to 65 % of the proof load, see Annex B.

e The prevailing torques for first assembly apply for all metal type nuts only. For prevailing torque non-metallic insert type nuts, the maximum torques shall be 50 % of the values.

Values in this table are required for testing performed under laboratory acceptance test conditions. Utilization of this type of fastener is application dependent and performance for parts may vary in normal use. It is recommended that additional testing of complete joints, using production components, be performed when there are questions of product performance.

Table 2 — Test clamp force and prevailing torques for prevailing torque type nuts of property class 05

| | Test clamp force | of total friction | Clamp force for evaluation of total friction coefficient $\mu_{\text{tot}}^{\text{b}}$ | | Prevailing torque N⋅m | | |
|----------|---------------------|-------------------|--|--------------------------|--------------------------|---------------------|--|
| Thread | | μ_{to} | ot I | | | 1 | |
| d P | F_{80}^{a} | Upper limit | Lower limit | 1st installation | 1st removal | 5th removal | |
| | N | F_{75}^{c} | F_{65}^{d} | $T_{\sf Fv,max}^{\sf e}$ | $T_{Fd,min}^{\qquad f}$ | $T_{Fd,min}^{f}$ | |
| | | N | N | ¹ Fv,max | ¹ Fd,min | ¹ Fd,min | |
| M3 | 2 000 | 1 875 | 1 625 | 0,6 | 0,15 | 0,1 | |
| M4 | 3 520 | 3 300 | 2 860 | 1,2 | 0,22 | 0,15 | |
| M5 | 5 680 | 5 325 | 4 615 | 2,1 | 0,35 | 0,24 | |
| M6 | 8 000 | 7 500 | 6 500 | 4 | 0,55 | 0,4 | |
| M7 | 11 600 | 10 875 | 9 425 | 6 | 0,85 | 0,6 | |
| M8 | 14 640 | 13 725 | 11 895 | 0 | 4.45 | 0.0 | |
| M8×1 | 15 680 | 14 700 | 12 740 | 8 | 1,15 | 0,8 | |
| M10 | 23 200 | 21 750 | 18 850 | | | | |
| M10×1,25 | 24 480 | 22 950 | 19 890 | 14 | 2 | 1,4 | |
| M10×1 | 25 760 | 24 150 | 20 930 | | | | |
| M12 | 33 760 | 31 650 | 27 430 | | 3,1 | | |
| M12×1,5 | 35 200 | 33 000 | 28 600 | 21 | | 2,1 | |
| M12×1,25 | 36 800 | 34 500 | 29 900 | | | | |
| M14 | 46 000 | 43 125 | 37 375 | 0.4 | 4.4 | 0 | |
| M14×1,5 | 50 000 | 46 875 | 40 625 | 31 | 4,4 | 3 | |
| M16 | 62 800 | 58 875 | 51 025 | 40 | 6 | 4.0 | |
| M16×1,5 | 66 800 | 62 625 | 54 275 | 42 | 6 | 4,2 | |
| M18 | 76 800 | 72 000 | 62 400 | 50 | _ | | |
| M18×1,5 | 86 000 | 80 625 | 69 875 | 56 | 8 | 5,5 | |
| M20 | 98 000 | 91 875 | 79 625 | 70 | 10.5 | _ | |
| M20×1,5 | 108 800 | 102 000 | 88 400 | 72 | 10,5 | 7 | |
| M22 | 121 200 | 113 625 | 98 475 | 00 | 40 | | |
| M22×1,5 | 133 200 | 124 875 | 108 225 | 90 | 13 | 9 | |
| M24 | 141 200 | 132 375 | 114 725 | 400 | 45 | 10.5 | |
| M24×2 | 153 600 | 144 000 | 124 800 | 106 | 15 | 10,5 | |
| M27 | 183 600 | 172 125 | 149 175 | 100 | 17 | 10 | |
| M27×2 | 198 400 | 186 000 | 161 200 | 123 | 17 | 12 | |
| M30 | 224 400 | 210 375 | 182 325 | 440 | 40 | 4.4 | |
| M30×2 | 248 400 | 232 875 | 201 825 | 140 | 19 | 14 | |
| M33 | 277 600 | 260 250 | 225 550 | 160 | 21 F | 15.5 | |
| M33×2 | 304 400 | 285 375 | 247 325 | | 21,5 15, | 10,5 | |
| M36 | 326 800 | 306 375 | 265 525 | 100 | 24 | 17.5 | |
| M36×3 | 346 000 | 324 375 | 281 125 | 180 | 24 | 17,5 | |
| M39 | 390 400 | 366 000 | 317 200 | 200 | 26.5 | 10.5 | |
| M39×3 | 412 000 | 386 250 | 334 750 | 200 | 26,5 | 19,5 | |

The clamp force for property class 05 nuts is equal to 80 % of the proof load of property class 05 nuts for 3 mm $\leq d \leq$ 39 mm. Proof loads for nuts are given in ISO 898-2 and ISO 898-6.

b See Annex B.

The value of the upper limit of the clamp force is equal to 75 % of the proof load, see Annex B.

The value of the lower limit of the clamp force is equal to 65 % of the proof load, see Annex B.

e The prevailing torques for first assembly apply for all metal type nuts only. For prevailing torque non-metallic insert type nuts, the maximum torques shall be 50 % of the values.

f Values in this table are required for testing performed under laboratory acceptance test conditions. Utilization of this type of fastener is application dependent and performance for parts may vary in normal use. It is recommended that additional testing of complete joints, using production components, be performed when there are questions of product performance.

Table 3 — Test clamp force and prevailing torques for prevailing torque type nuts of property class 5

| Thread | Test clamp force | Clamp force for evaluation of total friction coefficient $\mu_{ m tot}^{ m b}$ | | Prevailing torque N⋅m | | |
|----------|------------------------------|--|-----------------------------------|--------------------------|--------------------|--------------------|
| d P | F ₈₀ ^a | Upper limit | Lower limit | 1st installation | 1st removal | 5th removal |
| | N | F ₇₅ ^c N | F ₆₅ ^d N | $T_{Fv,max}^{}e}$ | $T_{Fd,min}{}^{f}$ | $T_{Fd,min}{}^{f}$ |
| M3 | 1 528 | 1 433 | 1 242 | 0,43 | 0,12 | 0,08 |
| M4 | 2 672 | 2 505 | 2 171 | 0,9 | 0,18 | 0,12 |
| M5 | 4 320 | 4 050 | 3 510 | 1,6 | 0,29 | 0,2 |
| M6 | 6 112 | 5 730 | 4 966 | 3 | 0,45 | 0,3 |
| M7 | 8 800 | 8 250 | 7 150 | 4,5 | 0,65 | 0,45 |
| M8 | 11 120 | 10 425 | 9 035 | | 0.05 | |
| M8×1 | 11 920 | 11 175 | 9 685 | 6 | 0,85 | 0,6 |
| M10 | 17 600 | 16 500 | 14 300 | | | |
| M10×1,25 | 18 640 | 17 475 | 15 145 | 10,5 | 1,5 | 1 |
| M10×1 | 19 600 | 18 375 | 15 925 | | • | |
| M12 | 25 600 | 24 000 | 20 800 | | 2,3 | |
| M12×1,5 | 26 800 | 25 125 | 21 775 | 15,5 | | 1,6 |
| M12×1,25 | 28 000 | 26 250 | 22 750 | | | |
| M14 | 34 960 | 32 775 | 28 405 | 0.4 | | |
| M14×1,5 | 38 000 | 35 625 | 30 875 | 24 | 3,3 | 2,3 |
| M16 | 47 760 | 44 775 | 38 805 | 00 | 4.5 | _ |
| M16×1,5 | 50 800 | 47 625 | 41 275 | 32 | 4,5 | 3 |
| M18 | 58 400 | 54 750 | 47 450 | 40 | • | 4.0 |
| M18×1,5 | 65 680 | 61 575 | 53 365 | 42 | 6 | 4,2 |
| M20 | 74 480 | 69 825 | 60 515 | | | |
| M20×1,5 | 82 400 | 77 250 | 66 950 | 54 | 7,5 | 5,3 |
| M22 | 92 000 | 86 250 | 74 750 | 00 | 2.5 | 0.5 |
| M22×1,5 | 100 800 | 94 500 | 81 900 | 68 | 9,5 | 6,5 |
| M24 | 107 200 | 100 500 | 87 100 | 00 | 44.5 | 0 |
| M24×2 | 116 800 | 109 500 | 94 900 | 80 | 11,5 | 8 |
| M27 | 113 600 | 106 500 | 92 300 | 0.4 | 40.5 | 40 |
| M27×2 | 123 200 | 115 500 | 100 100 | 94 | 13,5 | 10 |
| M30 | 139 200 | 130 500 | 113 100 | 400 | 40 | 40 |
| M30×2 | 153 600 | 144 000 | 124 800 | 108 | 16 | 12 |
| M33 | 172 000 | 161 250 | 139 750 | 122 | 40 | 4.4 |
| M33×2 | 188 800 | 177 000 | 153 400 | | 18 | 14 |
| M36 | 202 400 | 189 750 | 164 450 | 400 | 04 | 40 |
| M36×3 | 214 400 | 201 000 | 174 200 | 136 | 21 | 16 |
| M39 | 242 400 | 227 250 | 196 950 | 450 | 22 | 40 |
| M39×3 | 255 200 | 239 250 | 207 350 | 150 | 23 | 18 |

The clamp force for property class 5 nuts is equal to 80 % of the proof load of property class 5.8 bolts for 3 mm $\leq d \leq$ 24 mm, and 80 % of the proof load of property class 4.8 bolts for d > 24 mm. Proof loads for bolts are given in ISO 898-1.

b See Annex B.

The value of the upper limit of the clamp force is equal to 75 % of the proof load, see Annex B.

The value of the lower limit of the clamp force is equal to 65 % of the proof load, see Annex B.

e The prevailing torques for first assembly apply for all metal type nuts only. For prevailing torque non-metallic insert type nuts, the maximum torques shall be 50 % of the values.

Values in this table are required for testing performed under laboratory acceptance test conditions. Utilization of this type of fastener is application dependent and performance for parts may vary in normal use. It is recommended that additional testing of complete joints, using production components, be performed when there are questions of product performance.

Table 4 — Test clamp force and prevailing torques for prevailing torque type nuts of property class 6

| | Test clamp force | Clamp force for evaluation of total friction coefficient | | Prevailing torque | | | |
|----------|------------------|--|--------------|-------------------|--------------------------------|--------------------------------|--|
| Thread | 1 | μ_{t} | b tot | | N⋅m | | |
| d P | F_{80}^{a} | Upper limit | Lower limit | 1st installation | 1st removal | 5th removal | |
| | N | F ₇₅ ^c | F_{65}^{d} | | | | |
| | | N | N | $T_{Fv,max}^{}e}$ | $T_{Fd,min}^{\qquad \qquad f}$ | $T_{Fd,min}^{\qquad \qquad f}$ | |
| M3 | 1 768 | 1 658 | 1 437 | 0,43 | 0,12 | 0,08 | |
| M4 | 3 088 | 2 895 | 2 509 | 0,9 | 0,18 | 0,12 | |
| M5 | 5 000 | 4 688 | 4 063 | 1,6 | 0,29 | 0,2 | |
| M6 | 7 072 | 6 630 | 5 746 | 3 | 0,45 | 0,3 | |
| M7 | 10 160 | 9 525 | 8 255 | 4,5 | 0,65 | 0,45 | |
| M8 | 12 880 | 12 075 | 10 465 | | 0.05 | 0.0 | |
| M8×1 | 13 760 | 12 900 | 11 180 | 6 | 0,85 | 0,6 | |
| M10 | 20 400 | 19 125 | 16 575 | | | | |
| M10×1,25 | 21 520 | 20 175 | 17 485 | 10,5 | 1,5 | 1 | |
| M10×1 | 22 720 | 21 300 | 18 460 | 1 | , | | |
| M12 | 29 680 | 27 825 | 24 115 | | 2,3 | | |
| M12×1,5 | 31 040 | 29 100 | 25 220 | 15,5 | | 1,6 | |
| M12×1,25 | 32 400 | 30 375 | 26 325 | 1 | | | |
| M14 | 40 480 | 37 950 | 32 890 | | 3,3 | 2,3 | |
| M14×1,5 | 44 000 | 41 250 | 35 750 | 24 | | | |
| M16 | 55 280 | 51 825 | 44 915 | | | | |
| M16×1,5 | 58 800 | 55 125 | 47 775 | 32 | 4,5 | 3 | |
| M18 | 67 600 | 63 375 | 54 925 | 40 | 2 | 1.0 | |
| M18×1,5 | 76 000 | 71 250 | 61 750 | 42 | 6 | 4,2 | |
| M20 | 86 400 | 81 000 | 70 200 | | | 5.0 | |
| M20×1,5 | 96 000 | 90 000 | 78 000 | 54 | 7,5 | 5,3 | |
| M22 | 106 400 | 99 750 | 86 450 | 00 | 0.5 | 0.5 | |
| M22×1,5 | 116 800 | 109 500 | 94 900 | 68 | 9,5 | 6,5 | |
| M24 | 124 000 | 116 250 | 100 750 | 00 | 44.5 | | |
| M24×2 | 135 200 | 126 750 | 109 850 | 80 | 11,5 | 8 | |
| M27 | 161 600 | 151 500 | 131 300 | 6.1 | 40.5 | 40 | |
| M27×2 | 174 400 | 163 500 | 141 700 | 94 | 13,5 | 10 | |
| M30 | 197 600 | 185 250 | 160 550 | 400 | 40 | 40 | |
| M30×2 | 218 400 | 204 750 | 177 450 | 108 | 16 | 12 | |
| M33 | 244 000 | 228 750 | 198 250 | 400 | 40 | 4.4 | |
| M33×2 | 268 000 | 251 250 | 217 750 | 122 | 18 | 14 | |
| M36 | 287 200 | 269 250 | 233 350 | 400 | 0.1 | 40 | |
| M36×3 | 304 800 | 285 750 | 247 650 | 136 | 21 | 16 | |
| M39 | 343 200 | 321 750 | 278 850 | 1== | 0.5 | | |
| M39×3 | 362 400 | 339 750 | 294 450 | 150 | 23 | 18 | |

The clamp force for property class 6 nuts is equal to 80 % of the proof load of property class 6.8 bolts. Proof loads for bolts are given in ISO 898-1.

b See Annex B.

The value of the upper limit of the clamp force is equal to 75 % of the proof load, see Annex B.

The value of the lower limit of the clamp force is equal to 65 % of the proof load, see Annex B.

e The prevailing torques for first assembly apply for all metal type nuts only. For prevailing torque non-metallic insert type nuts, the maximum torques shall be 50 % of the values.

f Values in this table are required for testing performed under laboratory acceptance test conditions. Utilization of this type of fastener is application dependent and performance for parts may vary in normal use. It is recommended that additional testing of complete joints, using production components, be performed when there are questions of product performance.

Table 5 — Test clamp force and prevailing torques for prevailing torque type nuts of property class 8

| Thread | Test clamp force F_{80}^{a} | Clamp force for evaluation of total friction coefficient $\mu_{\rm tot}^{\ \ b}$ | | Prevailing torque | | | |
|----------|-------------------------------|--|--------------------------------|-------------------|--------------------------------|--------------------------------|--|
| d P | N N | Upper limit F_{75}^{c} | Lower limit $F_{65}{}^{\rm d}$ | 1st installation | 1st removal | 5th removal | |
| | | N | N | $T_{Fv,max}^{}}$ | $T_{Fd,min}^{\qquad \qquad f}$ | $T_{Fd,min}^{\qquad \qquad f}$ | |
| M3 | 2 336 | 2 190 | 1 898 | 0,43 | 0,12 | 0,08 | |
| M4 | 4 080 | 3 825 | 3 315 | 0,9 | 0,18 | 0,12 | |
| M5 | 6 584 | 6 173 | 5 350 | 1,6 | 0,29 | 0,2 | |
| M6 | 9 280 | 8 700 | 7 540 | 3 | 0,45 | 0,3 | |
| M7 | 13 440 | 12 600 | 10 920 | 4,5 | 0,65 | 0,45 | |
| M8 | 16 960 | 15 900 | 13 780 | | 0.05 | 0.0 | |
| M8×1 | 18 160 | 17 025 | 14 755 | 6 | 0,85 | 0,6 | |
| M10 | 26 960 | 25 275 | 21 905 | | | | |
| M10×1,25 | 28 400 | 26 625 | 23 075 | 10,5 | 1,5 | 1 | |
| M10×1 | 29 920 | 28 050 | 24 310 | † | | | |
| M12 | 39 120 | 36 675 | 31 785 | | 2,3 | | |
| M12×1,5 | 40 880 | 38 325 | 33 215 | 15,5 | | 1,6 | |
| M12×1,25 | 42 720 | 40 050 | 34 710 | <u> </u> | | | |
| M14 | 53 360 | 50 025 | 43 355 | | 3,3 | 0.0 | |
| M14×1,5 | 58 000 | 54 375 | 47 125 | 24 | | 2,3 | |
| M16 | 72 800 | 68 250 | 59 150 | 00 | | | |
| M16×1,5 | 77 520 | 72 675 | 62 985 | 32 | 4,5 | 3 | |
| M18 | 92 000 | 86 250 | 74 750 | 40 | | 4.2 | |
| M18×1,5 | 104 000 | 97 500 | 84 500 | 42 | 6 | 4,2 | |
| M20 | 117 600 | 110 250 | 95 550 | | | | |
| M20×1,5 | 130 400 | 122 250 | 105 950 | 54 | 7,5 | 5,3 | |
| M22 | 145 600 | 136 500 | 118 300 | 00 | 0.5 | 0.5 | |
| M22×1,5 | 160 000 | 150 000 | 130 000 | - 68 | 9,5 | 6,5 | |
| M24 | 169 600 | 159 000 | 137 800 | 00 | 44.5 | | |
| M24×2 | 184 000 | 172 500 | 149 500 | 80 | 11,5 | 8 | |
| M27 | 220 000 | 206 250 | 178 750 | 0.4 | 40.5 | 40 | |
| M27×2 | 238 400 | 223 500 | 193 700 | 94 | 13,5 | 10 | |
| M30 | 269 600 | 252 750 | 219 050 | 400 | 40 | 40 | |
| M30×2 | 298 400 | 279 750 | 242 450 | 108 | 16 | 12 | |
| M33 | 332 800 | 312 000 | 270 400 | 122 | 40 | 4.4 | |
| M33×2 | 365 600 | 342 750 | 297 050 | | 18 | 14 | |
| M36 | 392 000 | 367 500 | 318 500 | 400 | 0.1 | 40 | |
| M36×3 | 415 200 | 389 250 | 337 350 | 136 | 21 | 16 | |
| M39 | 468 800 | 439 500 | 380 900 | 450 | 00 | 40 | |
| M39×3 | 494 400 | 463 500 | 401 700 | 150 | 23 | 18 | |

a The clamp force for property class 8 nuts is equal to 80 % of the proof load of property class 8.8 bolts. Proof loads for bolts are given in ISO 898-1.

b See Annex B.

The value of the upper limit of the clamp force is equal to 75 % of the proof load, see Annex B.

d The value of the lower limit of the clamp force is equal to 65 % of the proof load, see Annex B.

e The prevailing torques for first assembly apply for all metal type nuts only. For prevailing torque non-metallic insert type nuts, the maximum torques shall be 50 % of the values.

Values in this table are required for testing performed under laboratory acceptance test conditions. Utilization of this type of fastener is application dependent and performance for parts may vary in normal use. It is recommended that additional testing of complete joints, using production components, be performed when there are questions of product performance.

Table 6 — Test clamp force and prevailing torques for prevailing torque type nuts of property class 9

| Thread d P | Test clamp force | Clamp force for evaluation of total friction coefficient $\mu_{\mathrm{tot}}^{\ \ \mathrm{b}}$ | | Prevailing torque N⋅m | | |
|----------------------|-----------------------------------|--|----------------------------------|---|--|--|
| | F ₈₀ ^a N | Upper limit F_{75}^{c} N | Lower limit $F_{65}{}^{\rm d}$ N | 1st installation ${T_{\rm Fv,max}}^{\rm e}$ | 1st removal $T_{\rm Fd,min}^{\qquad \qquad \rm f}$ | 5th removal $T_{\rm Fd,min}{}^{\rm f}$ |
| M3 | 2 616 | 2 453 | 2 126 | 0,43 | 0,12 | 0,08 |
| M4 | 4 568 | 4 283 | 3 712 | 0,9 | 0,18 | 0,12 |
| M5 | 7 384 | 6 923 | 6 000 | 1,6 | 0,29 | 0,2 |
| M6 | 10 480 | 9 825 | 8 515 | 3 | 0,45 | 0,3 |
| M7 | 15 040 | 14 100 | 12 220 | 4,5 | 0,65 | 0,45 |
| M8 | 19 040 | 17 850 | 15 470 | 6 | 0,85 | 0.6 |
| M8×1 | 20 400 | 19 125 | 16 575 | 6 | | 0,6 |
| M10 | 30 160 | 28 275 | 24 505 | | | |
| M10×1,25 | 31 840 | 29 850 | 25 870 | 10,5 | 1,5 | 1 |
| M10×1 | 33 520 | 31 425 | 27 235 | ┦ | | |
| M12 | 43 840 | 41 100 | 35 620 | | | |
| M12×1,5 | 45 840 | 42 975 | 37 245 | 15,5 | 2,3 | 1,6 |
| M12×1,25 | 47 920 | 44 925 | 38 935 | 1 | | |
| M14 | 59 840 | 56 100 | 48 620 | 24 | 2.2 | 2.2 |
| M14×1,5 | 64 960 | 60 900 | 52 780 | 24 | 3,3 | 2,3 |
| M16 | 81 600 | 76 500 | 66 300 | 32 | 4.5 | 2 |
| M16×1,5 | 87 200 | 81 750 | 70 850 | 32 | 4,5 | 3 |

The clamp force for property class 9 nuts is equal to 80 % of the proof load of property class 9.8 bolts. Proof loads for bolts are given in ISO 898-1.

b See Annex B.

The value of the upper limit of the clamp force is equal to 75 % of the proof load, see Annex B.

The value of the lower limit of the clamp force is equal to 65 % of the proof load, see Annex B.

e The prevailing torques for first assembly apply for all metal type nuts only. For prevailing torque non-metallic insert type nuts, the maximum torques shall be 50 % of the values.

f Values in this table are required for testing performed under laboratory acceptance test conditions. Utilization of this type of fastener is application dependent and performance for parts may vary in normal use. It is recommended that additional testing of complete joints, using production components, be performed when there are questions of product performance.

Table 7 — Test clamp force and prevailing torques for prevailing torque type nuts of property class 10

| Thread | Test clamp force | Clamp force for evaluation of total friction coefficient $\mu_{\mathrm{tot}}^{\ \ \mathrm{b}}$ | | Prevailing torque N⋅m | | |
|----------|-----------------------------------|--|--------------------------------|---|------------------------------|------------------------------|
| d P | F ₈₀ ^a N | Upper limit F_{75}^{c} | Lower limit $F_{65}{}^{\rm d}$ | 1st installation $T_{Fv,max}^{\qquad \qquad e}$ | 1st removal $T_{Fd,min}^{}}$ | 5th removal $T_{Fd,min}^{f}$ |
| | 2011 | N | N | | | |
| M3 | 3 344 | 3 135 | 2 717 | 0,6 | 0,15 | 0,1 |
| M4 | 5 832 | 5 468 | 4 739 | 1,2 | 0,22 | 0,15 |
| M5 | 9 440 | 8 850 | 7 670 | 2,1 | 0,35 | 0,24 |
| M6 | 13 360 | 12 525 | 10 855 | 4 | 0,55 | 0,4 |
| M7 | 19 200 | 18 000 | 15 600 | 6 | 0,85 | 0,6 |
| M8 | 24 320 | 22 800 | 19 760 | 8 | 1,15 | 0,8 |
| M8×1 | 26 000 | 24 375 | 21 125 | | | |
| M10 | 38 480 | 36 075 | 31 265 | _ | | |
| M10×1,25 | 40 640 | 38 100 | 33 020 | 14 | 2 | 1,4 |
| M10×1 | 42 800 | 40 125 | 34 775 | | | |
| M12 | 56 000 | 52 500 | 45 500 | | 3,1 | 2,1 |
| M12×1,5 | 58 480 | 54 825 | 47 515 | 21 | | |
| M12v1,25 | 61 120 | 57 300 | 49 660 | | | |
| M14 | 76 400 | 71 625 | 62 075 | 31 | 4,4 | 3 |
| M14×1,5 | 83 200 | 78 000 | 67 600 | 31 | 4,4 | |
| M16 | 104 000 | 97 500 | 84 500 | 40 | 6 | 4.0 |
| M16×1,5 | 111 200 | 104 250 | 90 350 | 42 | | 4,2 |
| M18 | 127 200 | 119 250 | 103 350 | 50 | 8 | 5,5 |
| M18×1,5 | 143 200 | 134 250 | 116 350 | 56 | | |
| M20 | 162 400 | 152 250 | 131 950 | | 40 = | _ |
| M20×1,5 | 180 800 | 169 500 | 146 900 | 72 | 10,5 | 7 |
| M22 | 201 600 | 189 000 | 163 800 | | | _ |
| M22×1,5 | 220 800 | 207 000 | 179 400 | 90 | 13 | 9 |
| M24 | 234 400 | 219 750 | 190 450 | 100 | | 10.5 |
| M24×2 | 255 200 | 239 250 | 207 350 | 106 | 15 | 10,5 |
| M27 | 304 800 | 285 750 | 247 650 | 455 | | |
| M27×2 | 329 600 | 309 000 | 267 800 | 123 | 17 | 12 |
| M30 | 372 800 | 349 500 | 302 900 | 4 | | |
| M30×2 | 412 000 | 386 250 | 334 750 | 140 | 19 | 14 |
| M33 | 460 800 | 432 000 | 374 400 | 160 | | |
| M33×2 | 505 600 | 474 000 | 410 800 | | 21,5 | 15,5 |
| M36 | 542 400 | 508 500 | 440 700 | 455 | | |
| M36×3 | 574 400 | 538 500 | 466 700 | 180 | 24 | 17,5 |
| M39 | 648 000 | 607 500 | 526 500 | | | |
| M39×3 | 684 000 | 641 250 | 555 750 | 200 | 26,5 | 19,5 |

The clamp force for property class 10 nuts is equal to 80 % of the proof load of property class 10.9 bolts. Proof loads for bolts are given in ISO 898-1.

b See Annex B.

The value of the upper limit of the clamp force is equal to 75 % of the proof load, see Annex B.

The value of the lower limit of the clamp force is equal to 65 % of the proof load, see Annex B.

e The prevailing torques for first assembly apply for all metal type nuts only. For prevailing torque non-metallic insert type nuts, the maximum torques shall be 50 % of the values.

f Values in this table are required for testing performed under laboratory acceptance test conditions. Utilization of this type of fastener is application dependent and performance for parts may vary in normal use. It is recommended that additional testing of complete joints, using production components, be performed when there are questions of product performance.

Table 8 — Test clamp force and prevailing torques for prevailing torque type nuts of property class 12

| Thread d P | Test clamp force | Clamp force for evaluation of total friction coefficient $\mu_{\rm tot}^{\ \ b}$ | | Prevailing torque N·m | | |
|----------------------|-----------------------------------|--|----------------------------------|---|---------------------------------|---------------------------------|
| | F ₈₀ ^a N | Upper limit $F_{75}{}^{\rm c}$ N | Lower limit $F_{65}{}^{\rm d}$ N | 1st installation $T_{\rm Fv,max}^{ \ \ e}$ | 1st removal $T_{\rm Fd,min}^{}$ | 5th removal $T_{\rm Fd,min}^{}$ |
| M3 | 3 904 | 3 660 | 3 172 | 0,6 | 0,15 | 0,1 |
| M4 | 6 816 | 6 390 | 5 538 | 1,2 | 0,22 | 0,15 |
| M5 | 11 040 | 10 350 | 8 970 | 2,1 | 0,35 | 0,24 |
| M6 | 15 600 | 14 625 | 12 675 | 4 | 0,55 | 0,4 |
| M7 | 22 400 | 21 000 | 18 200 | 6 | 0,85 | 0,6 |
| M8 | 28 400 | 26 625 | 23 075 | 0 | 4.45 | 0.0 |
| M8×1 | 30 400 | 28 500 | 24 700 | 8 | 1,15 | 0,8 |
| M10 | 45 040 | 42 225 | 36 595 | | | |
| M10×1,25 | 47 520 | 44 550 | 38 610 | 14 | 2 | 1,4 |
| M10×1 | 50 160 | 47 025 | 40 755 | 1 | | |
| M12 | 65 440 | 61 350 | 53 170 | | 3,1 | |
| M12×1,5 | 68 400 | 64 125 | 55 575 | 21 | | 2,1 |
| M12×1,25 | 71 440 | 66 975 | 58 045 | | | |
| M14 | 89 600 | 84 000 | 72 800 | 24 | 4,4 | 2 |
| M14×1,5 | 96 800 | 90 750 | 78 650 | 31 | | 3 |
| M16 | 121 600 | 114 000 | 98 800 | 42 | 6 | 4,2 |
| M16×1,5 | 129 600 | 121 500 | 105 300 | 42 | | |
| M18 | 148 800 | 139 500 | 120 900 | 56 | 8 | 5,5 |
| M18×1,5 | 168 000 | 157 500 | 136 500 | 50 | 0 | |
| M20 | 190 400 | 178 500 | 154 700 | 72 | 10.5 | 7 |
| M20×1,5 | 211 200 | 198 000 | 171 600 | 12 | 10,5 | / |
| M22 | 235 200 | 220 500 | 191 100 | 90 | 13 | 9 |
| M22×1,5 | 258 400 | 242 250 | 209 950 | 90 | 13 | 9 |
| M24 | 273 600 | 256 500 | 222 300 | 106 | 15 | 10,5 |
| M24×2 | 297 600 | 279 000 | 241 800 | 100 | 15 | 10,5 |
| M27 | 356 000 | 333 750 | 289 250 | 123 | 17 | 12 |
| M27×2 | 384 800 | 360 750 | 312 650 | 123 | 17 | 12 |
| M30 | 435 200 | 408 000 | 353 600 | 140 | 19 | 14 |
| M30×2 | 481 600 | 451 500 | 391 300 | 140 | | 14 |
| M33 | 538 400 | 504 750 | 374 400 | 160 | 21,5 | 15,5 |
| M33×2 | 590 400 | 553 500 | 479 700 | | ۵,۱۵ | 15,5 |
| M36 | 633 600 | 594 000 | 514 800 | 190 | 24 | 17 F |
| M36×3 | 671 200 | 629 250 | 545 350 | 180 | 24 | 17,5 |
| M39 | 757 600 | 710 250 | 615 550 | 200 | 26.5 | 10.5 |
| M39×3 | 799 200 | 749 250 | 649 350 | 200 | 26,5 | 19,5 |

The clamp force for property class 12 nuts is equal to 80 % of the proof load of property class 12.9 bolts. Proof loads for bolts are given in ISO 898-1.

b See Annex B.

The value of the upper limit of the clamp force is equal to 75 % of the proof load, see Annex B.

The value of the lower limit of the clamp force is equal to 65 % of the proof load, see Annex B.

e The prevailing torques for first assembly apply for all metal type nuts only. For prevailing torque non-metallic insert type nuts, the maximum torques shall be 50 % of the values.

f Values in this table are required for testing performed under laboratory acceptance test conditions. Utilization of this type of fastener is application dependent and performance for parts may vary in normal use. It is recommended that additional testing of complete joints, using production components, be performed when there are questions of product performance.

9 Test method

9.1 General

The nuts shall be tested as received.

9.2 Proof load test

The proof load test shall be carried out according to ISO 898-2 or ISO 898-6. Additionally, the following applies.

The nut to be tested shall be assembled on a test bolt (see 9.3) or on a hardened steel mandrel. The maximum prevailing torque to assemble the nut through 360° rotation shall be recorded after the first full thread has passed through the prevailing torque feature and assembly continues until three full threads protrude through the nut. For referee test purposes, a hardened steel mandrel shall be used for prevailing torque non-metallic insert type nuts and a test bolt shall be used for prevailing torque all metal type nuts. The maximum prevailing torque occurring during the assembly of the nut on the test bolt or mandrel shall be recorded after the first full form thread has passed through the prevailing torque feature.

A load equal to the specified proof load for the nut, as specified in ISO 898-2 or ISO 898-6, shall be applied through the test bolt or mandrel against the nut-bearing surface in an axial direction and shall be held for 15 s. The nut shall resist this load without thread stripping or rupture. The proof load test is decisive.

The maximum prevailing torque occurring during disassembly of the nut after a half-turn to full disengagement measured with the nut in motion shall not exceed the recorded maximum prevailing torque during assembly.

9.3 Prevailing torque test

9.3.1 General

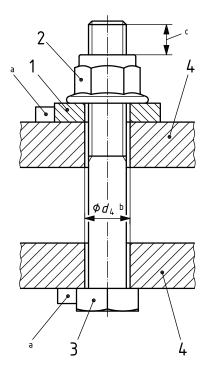
The purpose of this test method is to obtain simultaneously on the prevailing torque type nuts:

- a) the performance properties (prevailing torques developed by the nut);
- b) the torque/clamp force properties tested according to ISO 16047, when agreed between the manufacturer and the purchaser.

9.3.2 Test apparatus

For test apparatus, see ISO 16047.

For the test setup, see Figure 1. Test apparatus shall not generate clamp force during prevailing torque testing.



Key

- 1 test-bearing plate/washer
- 2 nut to be tested
- 3 test bolt/screw
- 4 load cell
- d_4 diameter of the hole of the fixture
- ^a Test-bearing plate or test washer and bolt head shall be fixed by suitable means to prevent rotation and shall be aligned.
- $^{\rm b}$ $d_{\rm 4}$ shall be in accordance with ISO 273:1979, fine series.
- c 4 to 7 pitches.

Figure 1 — Test setup and nut when seated

9.3.3 Test parts

For test bolts/screws and test plate/washer, see ISO 16047. The test bolt and test washer surface finish shall be in accordance with ISO 16047, plain surface uncoated and degreased, unless otherwise agreed. The test washer shall be of type HH, unless otherwise agreed. With the exception of the test mandrel, test parts shall be used only once.

The property class of the test bolt/screw shall be chosen according to Table 9.

Table 9 — Property classes for the test bolt/screw

| Nut to be tested | Corresponding test bolt/screw |
|------------------|-------------------------------|
| Property class | |
| 04 | ≽8.8 |
| 5 | ≥8.8 |
| 05 | ≥10.9 |
| 6 | ≥8.8 |
| 8 | ≥8.8 |
| 9 | ≥9.8 |
| 10 | ≽10.9 |
| 12 | 12.9 |

9.3.4 Test procedure

This test can be realized automatically on an appropriate testing device or manually with adequate hand tools like torque wrenches and load cells, see 9.3.2.

In case of dispute, the automatic mode applies.

Torque/clamp force testing conditions are specified in ISO 16047.

The test bolt/screw is placed in the testing device such that the protrusion through the prevailing torque feature of the nut after seating is according to Figure 1.

The nut to be tested is engaged by hand on the bolt/screw thread until the prevailing torque feature is engaged. The end of the test bolt/screw shall not protrude through the nut before testing. The threaded length for tightening shall be four to seven pitches according to Figure 1.

The starting point of the installation phase corresponds to the start-up of the tightening device (see point 1 in Figure 2).

The rotation shall be continuous and uniform from point 1 until the test clamp force, F_{80} , is reached. Values for F_{80} are given in Tables 1 to 8. Torque at clamp force F_{75} shall be recorded and evaluated.

NOTE The F_{80} value provides the shut-down signal for the test device to ensure precise evaluation at F_{75} .

The seating point (see point 2 in Figure 2) shall be determined. Between point 1 and point 2, the prevailing-on torque, $T_{\text{Fv,max}}$, shall be measured (see Tables 1 to 8).

The nut is then rotated off by the application of a reverse torque until the clamp force in the test bolt/screw is reduced to zero (see point 3 in Figure 2). The prevailing-off torque, $T_{\text{Fd,min}}$, occurring while the nut is rotated through the next 360° of rotation (see point 4 in Figure 2) shall be measured (see Tables 1 to 8). Point 4 corresponds to the angular position of point 3 minus 360°.

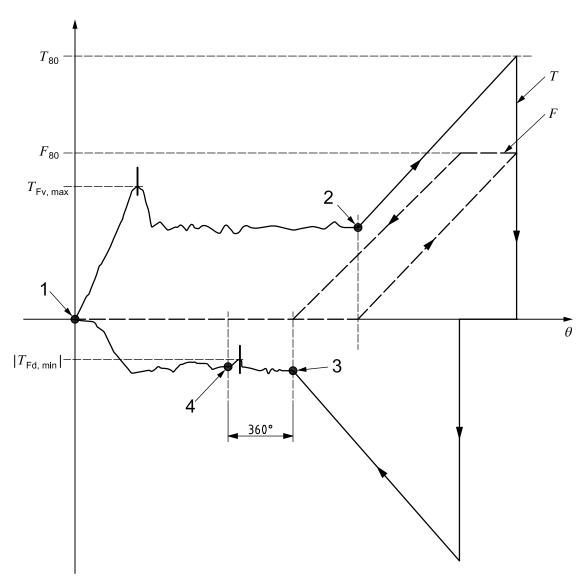
The nut is then disassembled until the initial angular position has reached the starting point (see point 1).

During the removal of the nut, the rotating shall be continuous and uniform from the test clamp force, F_{80} , to point 1.

After the complete removal of the nut, the nut and bolt threads shall not be damaged. In case of dispute, the test bolt shall accept the appropriate ring gauge.

For determination of the values for the 5th removal, the above procedure will be performed four more times between point 1 and point 2 only.

During the 5th removal, the prevailing-off torque occurring while the nut is being rotated through the first 360° shall be measured. This torque shall be equal to, or higher than, the 5th removal prevailing torque value as specified in Tables 1 to 8.



Key

- F clamp force
- T torque
- θ angle
- point where prevailing-on torque occurs first and measurement of $T_{\rm Fv}$ starts
- 2 seating point, end of measurement of T_{Fv}
- 3 no contact with the test plate/ washer, beginning of measurement of $T_{\rm Ed}$
- 4 end of measurement of T_{Fd}

Figure 2 — Torque/clamp force/angle curve

9.3.5 Test report

See ISO 16047 for an outline of the test report content. A reference to this International Standard shall be included in the test report.

The prevailing-on torque, $T_{\rm Fv}$, and the prevailing-off torque, $T_{\rm Fd}$, (and, if required, the temperature resistance test result for prevailing torque non-metallic insert type nuts) shall be included in the test report.

Annex A

(normative)

Temperature resistance of prevailing torque non-metallic insert type nuts

The specifications given in this annex may be agreed between customer and supplier, if appropriate.

At ambient temperature (10 °C to 35 °C), the nut shall be assembled on to a test bolt until four to seven full threads protrude through the top of the nut but no clamp force is induced.

The assembly shall be placed in a chamber at +120 °C; after 1 h, it shall be removed from the chamber to cool naturally to ambient temperature.

The assembly shall then be placed in a chamber at -50 °C; after 1 h, it shall be removed from the chamber to recover naturally to ambient temperature.

With the assembly at ambient temperature, the prevailing torque test according to the test procedure given in 9.3.4 shall be carried out, disregarding the prevailing-on torque and clamp force. The prevailing torques measured at the first and the fifth removal shall not be lower than the relevant values specified in Tables 1 to 8.

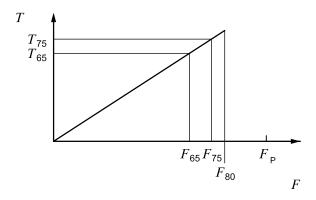
Upon agreement between customer and supplier, the temperature range may be modified to suit application requirements.

Annex B (informative)

Basis for the evaluation of the total coefficient of friction, μ_{tot}

The tightening process runs up to a test clamp force of 80 % of the proof load of the mating bolt. For evaluation of the coefficient of friction, μ_{tot} , the clamp force is determined at 65 % and 75 % of the proof load value.

The coefficient of friction, μ_{tot} , is calculated as the mean of the coefficient of friction at the upper limit and at the lower limit.



Key

 F_{80}

 T_{65} T_{75}

 F_{P} proof load

lower load limit for the evaluation of the coefficient of total friction at 65 % of $F_{\rm P}$ F_{65} F_{75}

upper load limit for the evaluation of the coefficient of total friction at 75 % of $F_{\rm p}$

test clamp force (shut-down force for the tightening process) at 80 % of $F_{\rm P}$

lower torque limit for the evaluation of the coefficient of total friction at F_{65}

upper torque limit for the evaluation of the coefficient of total friction at F_{75}

Figure B.1 — Principles for evaluation of the coefficient of friction, μ_{tot}

Bibliography

- [1] ISO 68-1, ISO general purpose screw threads Basic profile Part 1: Metric screw threads
- [2] ISO 261, ISO general purpose metric screw threads General plan
- [3] ISO 262, ISO general purpose metric screw threads Selected sizes for screws, bolts and nuts

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